LS-DYNA® Peridynamics for Brittle Failure Analysis

A new physical based theory to predict the mixed mode damage process in brittle solid

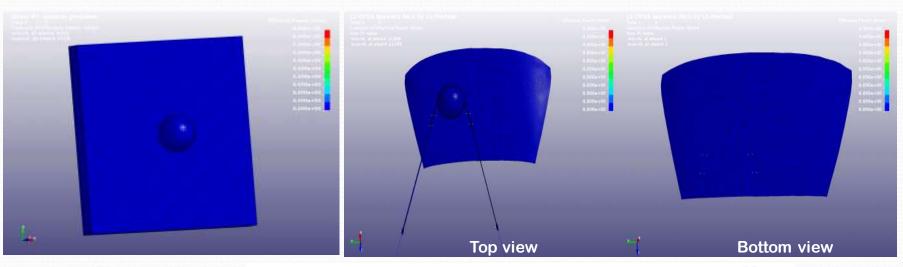
Bo Ren

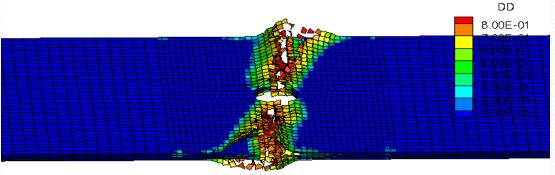
boren@lstc.com

Oct. 23, 2017 Shanghai, China



What is Peridynamics Designed for?





Complex damage evolution in brittle materials

Peridynamics Development History

- 1. Is a new nonlocal "theory" for material failure analysis.
- Has bond-based and state-based peridynamic theories.
- 3. Was developed by Dr. Steward Silling at Sandia Nat. Lab. in 2000.
- 4. Conventional bond-based and state-based peridynamics do not work well for non-uniform discretization and have difficulties to prescribe boundary conditions and kinematic constraints.
- 5. To bypass the numerical problems in 4., the bond-based peridynamics was implemented into LS-DYNA® using Discontinuous Galerkin (DG) Finite Element Method.
- 6. Only available in LS-DYNA (SMP/MPP) since 2016.

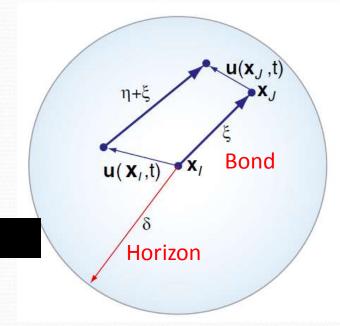
1. Peridynamic Theory

$$\rho \ddot{u_i}(X_I) = \sigma_{ij,j} + b_i(X_I) \quad \text{Classical local theory}$$

$$\rho \ddot{u_i}(X_I) = \int_{H_X} f_i < \eta_i, \xi_I > dV_{X'} + b_i(X_I)$$

$$\xi_I = X_I' - X_I$$

$$\eta_i = u_i^P - u_i$$



$$f = cs \frac{\eta + \xi}{|\eta + \xi|}, \quad s = \frac{|\xi + \eta| - |\xi|}{|\xi|}, \quad c = \frac{18K}{\pi \delta^4}$$

Here s is the bond stretch with micro modulus c. A bond will break permanently when its bond compression or tension over a critical value:

$$s \leq s_t \text{ or } s \geq s_c$$

breakage

Bond strain

- *SECTION_SOLID_PERI (Available in R10., MPP, SMP)
 - Card 1

Variable	SECID	ELFORM
Type	I	ı
Default		

ELFORM EQ.48: Peridynamic formulation for TET, PENT, HEX solid elements

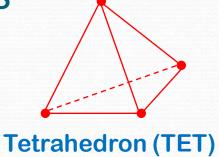
Card 2

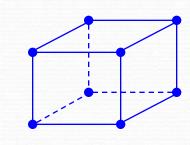
Variable	DR	PTYPE
Туре	F	l
Default	1.01	1

DR: normalized horizon size, $0.6 \sim 1.2$ is recommended

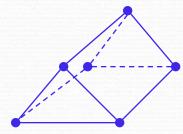
PTYPE EQ.1: bond based formulation

EQ.2: state based formulation



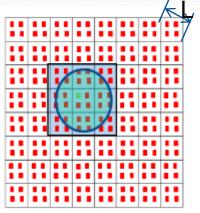


Hexahedron (HEX)



Pentahedron (PENT)

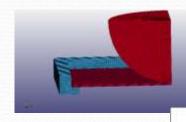
DR: the normalized support zone size



$$R = DR * L$$

DR is the user defined reference support size LSDYNA will adjust DR automatically to make sure the neighbors of a point is $10 \le n_a \le 136$

Warning. The maximum neighbor number is 36 the minimum neighbor number: 9 which violates the threshold: 10~136 (Min~Max). The horizon size will be tuned, and new search starts



Don't support the extremely poor mesh

- *MAT ELASTIC PERI (available in R10.0, MPP, SMP)
 - Card 1

Variab le	MID	RO	E	G_T	G_S
Туре	ı	ı	F	F	F
Defaul t				1.0E20	1.0e20

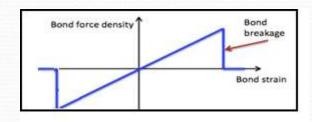
The only material type can be used for peridynamics.

RO: density

E: Young's modulus $E \rightarrow c$

 G_T : fracture energy release rate $G \rightarrow s_c$

*G*_s: fracture energy release rate for compression



Comments

 $G_s = 2.0 * G_T$ For compression problems

Nonconforming mesh leads to wrong results

Four ways to deal with peridynamic and FEM interface:

1) *CONTACT_AUTOMATIC_*.

Peridynamic parts can interact with other parts through regular contact.

*CONTACT_AUTOMATIC_NODES_TO_SUFRACE is recommended as peridynamic part is the slave part.

2) Sharing nodes at the interfaces

Merging all the nodes on the FEM-Peridynamic interfaces

Advantage: efficient

Disadvantage: the interface can not be separated.

3) *CONTACT_TIED_SURFACE_TO_SURFACE_OFFSET

Advantage: easy to use, the tie can break.

Disadvantage: expensive, sometimes unstable.

4) *CONTACT_FEM_PERI_TIE_opts

Advantage: efficient, the tie can break.

Disadvantage: require coincide nodes on the interface.

This key word requires coincide nodes on the interface.

3. The Keywords for Peridynamics

*CONTACT_FEM_PERI_TIE_opt (beta version, SMP)

This keyword will be changed to: *CONSTRAINED_FEM_PERI_TIE_opt

• Card 1

Variable	CID	MSID	SSID	FT	FS
Туре	I	ı	F	F	F
Default				1.0E20	1.0E20

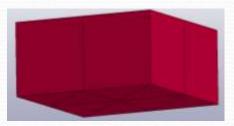
CID: Contact ID

MSID: The FEM part ID

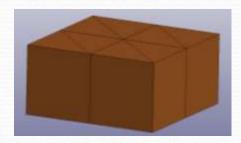
SSID: The peridynamic part ID

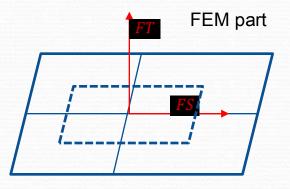
opt: BREAK

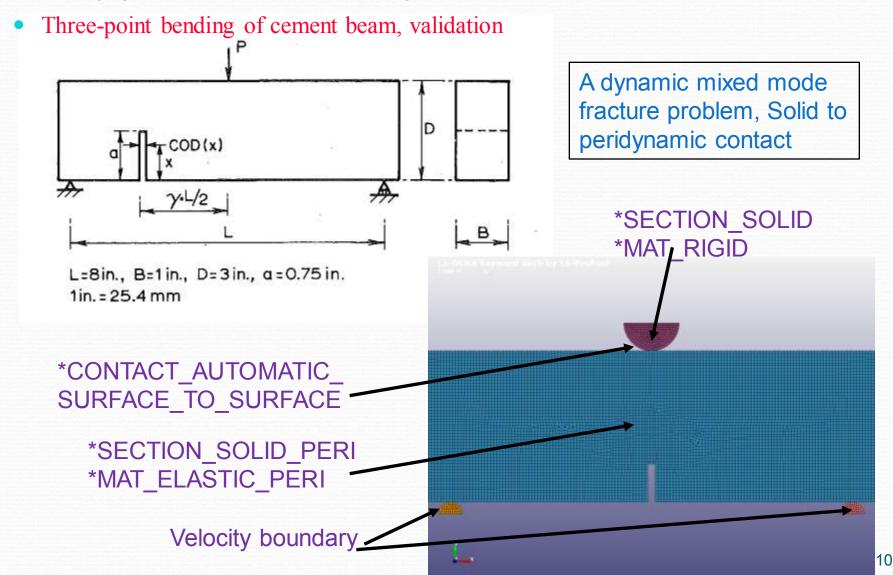
FT: The tensile stress to break the tie Fs: The shear stress to break the tie



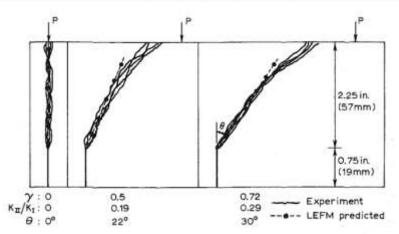
Peridynamic part



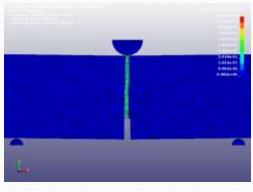




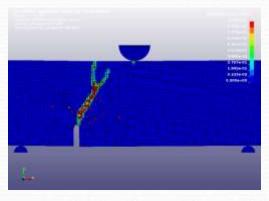
• Three-point bending of cement beam, validation



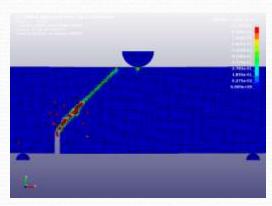
Experimental crack path from tension to mixture mode





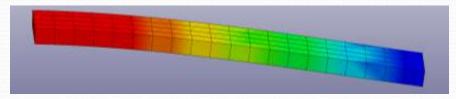




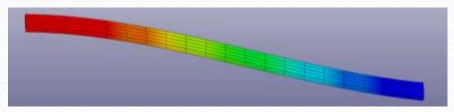


γ=0.7 Θ=29⁰

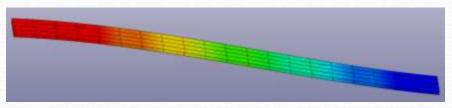
• Cantilever beam-High aspect ratio elements



•Thickness: 1.0

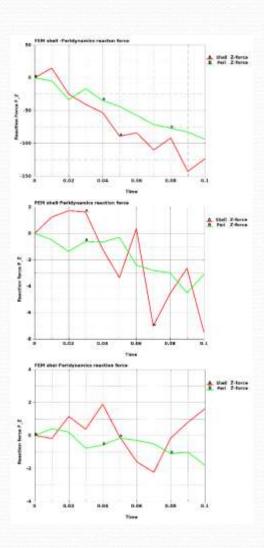


•Thickness: 0.3

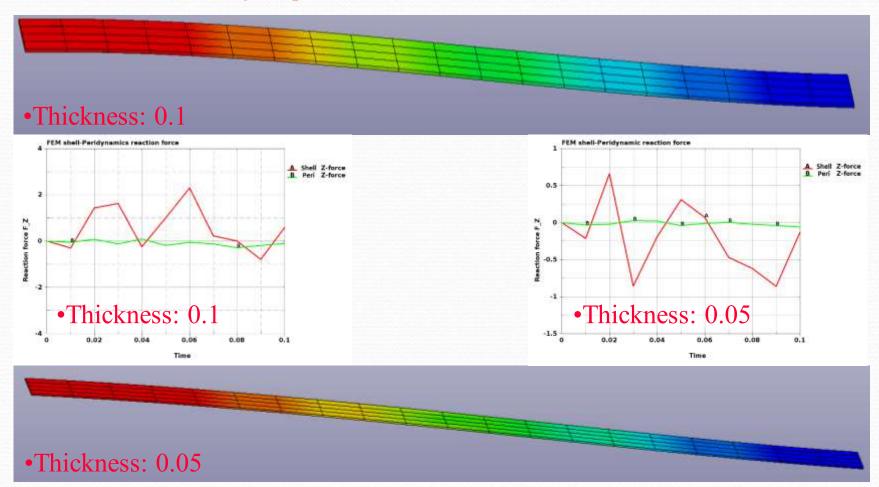


•Thickness: 0.2

*SECTION_SOLID_PERI *MAT_ELASTIC_PERI



• Cantilever beam-High aspect ratio elements

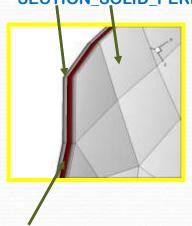


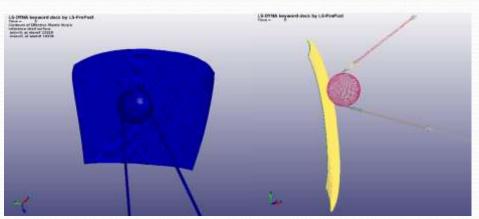
Windshield impact

Impact/penetration, FEM-Peridynamic parts tie

Glass layers: Peridynamic solid

*SECTION_SOLID_PERI, *MAT_ELASTIC_PERI





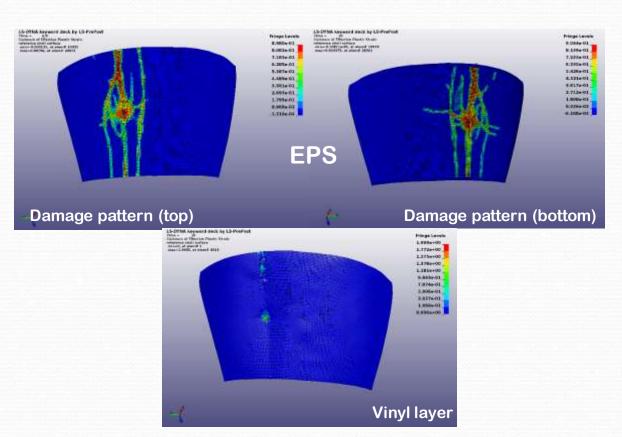
Vinyl layer: FEM solid

*MAT_PIECEWISE_LINEAR_PLASTICITY

Interface of vinyl and glasses:

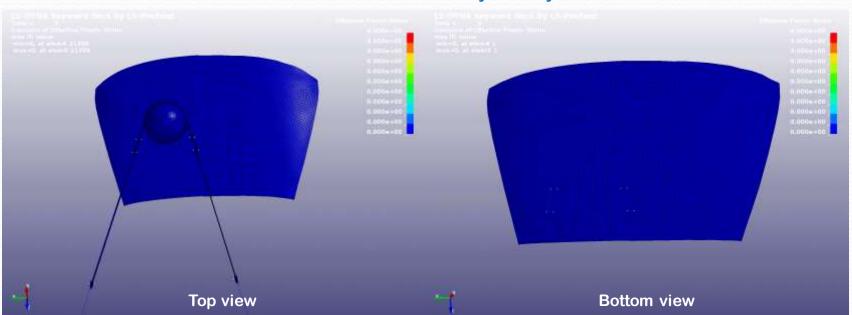
*CONTACT_TIED_SURFACE_TO_SURFACE_OFFSET

Windshield impact



Windshield impact

von Mises stress on vinyl interlayer

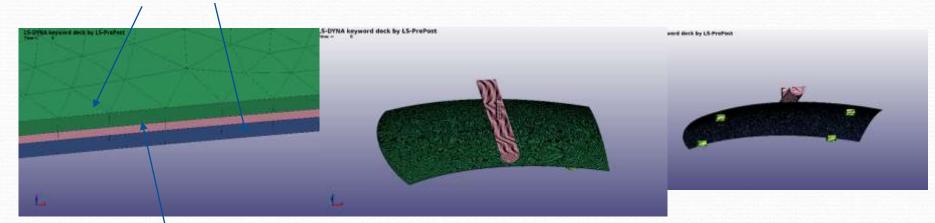


• Windshield: 3-point bending

Indentation failure, FEM-Peridynamic parts tie

Glass layers: Peridynamic solid

*SECTION_SOLID_PERI, *MAT_ELASTIC_PERI: GC=2.*GT



Vinyl layer: FEM solid

*MAT_PIECEWISE_LINEAR_PLASTICITY, fail EPS: 0.05, sigy:12.0

Interface of vinyl and glasses:

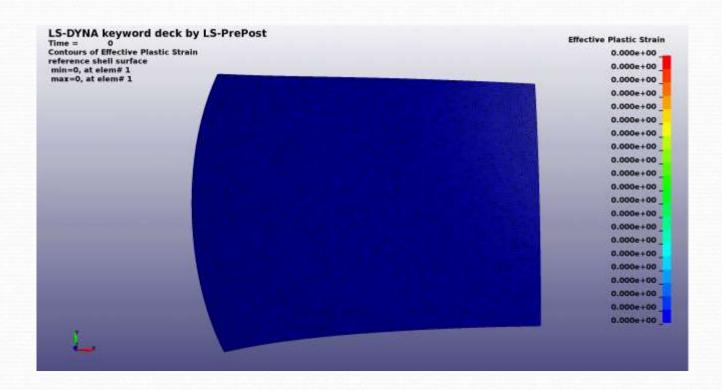
*CONTACT_FEM_PERI_TIE_BREAK, FT, FS=10.5

Contact between Impactor and glass layers:

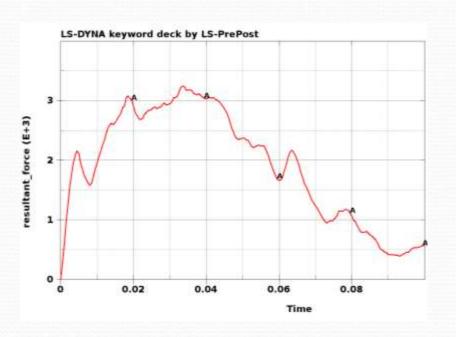
*CONTACT_AUTOMATIC_NODES_TO_SURFACE

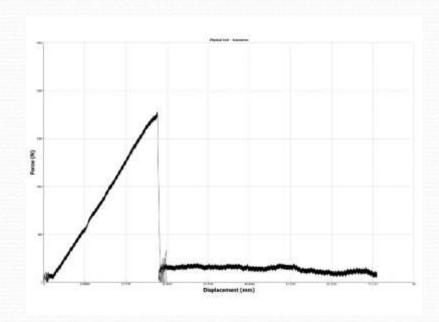
Contact between Supports and glass layers:

*CONTACT_AUTOMATIC_SURFACE_TO_SURFACE



Damage evolution





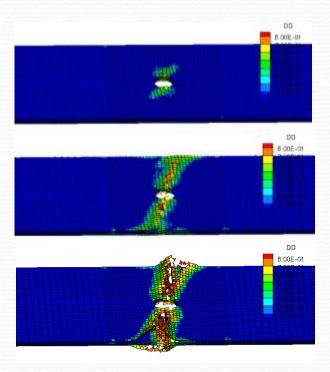
Numerical dynamic reaction force history

Experimental static reaction force history

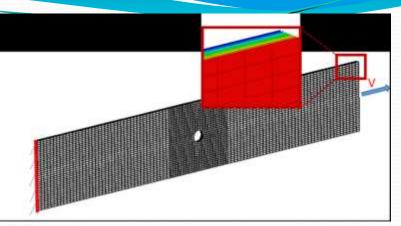
Maximum Force (N)		Displacement (mm)		
Exp.	Num.	Exp.	Num.	
2841	3250	24.6	16.7	

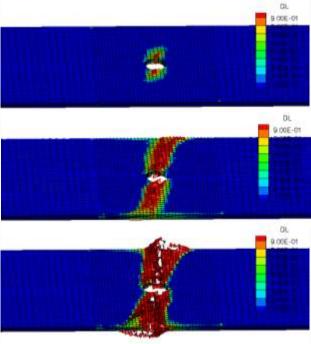
5. Future Work

- Fiber reinforced composite laminate
 - T700 carbon/epoxy material
 - Eight laminate [45/0/-45/90]s layers
 - 229504 nodes



Inner-layer failure





Delamination

Conclusion Remarks on the Peridynamics

- Current explicit dynamics version is mainly for brittle failure analysis.
- ☐ Is a discontinuous Galerkin (DG) approach with bond-based peridynamic theory.
- Failure is based on critical energy released rate. No element deletion is needed to advance the cracks.
- □ Branching of the cracks is an outcome of the DG approach. Self-contact between cracks is possible but CPU time consuming.
- Accommodates for non-uniform mesh and allow the direct enforcement of essential boundary conditions and constraints.
- ☐ A trial executable is available upon request. R10.0 support *SEC.._PERI and *MAT.._PERI
- ☐ In crashworthiness simulation, it is mainly for windshield and brittle panels damage analysis.

Thanks for your attention!

